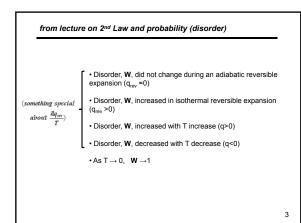
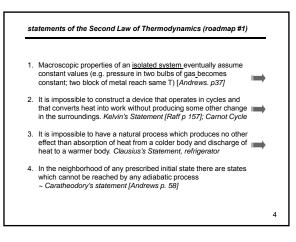
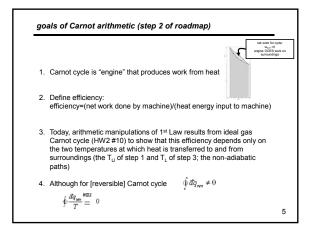
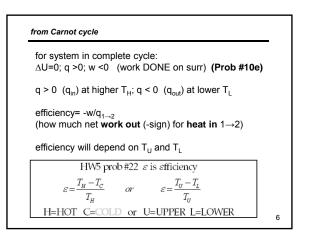


- 1. Phenomenological statements (what is ALWAYS observed)
- 2. Ideal gas Carnot [reversible] cycle efficiency of heat \to work (Carnot cycle transfers heat only at $\rm T_U$ and $\rm T_L$)
- Any cyclic engine operating between T_u and T_L must have an equal or lower efficiency than Carnot OR VIOLATE one of the phenomenological statements (observations)
- 4. Generalize Carnot to any reversible cycle (E&R fig 5.4)
- 5. Show that for this REVERSIBLE cycle $q_U + q_L \neq 0$ (dq inexact differential) but $\frac{dy}{T_U} + \frac{q_L}{T_L} = 0$ (something special about $\frac{dq_{rec}}{T}$)
- 6. S, entropy and spontaneous changes

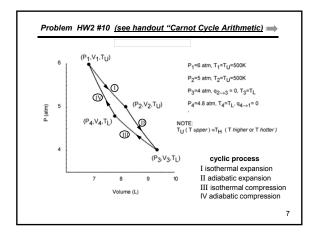


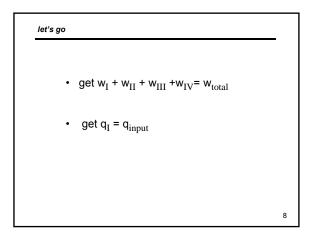




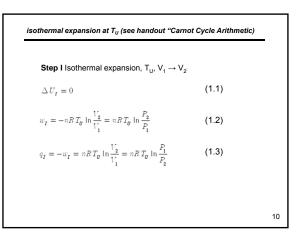


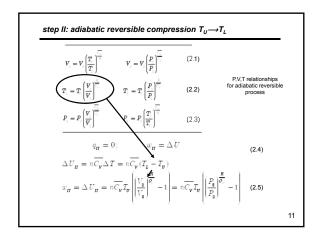
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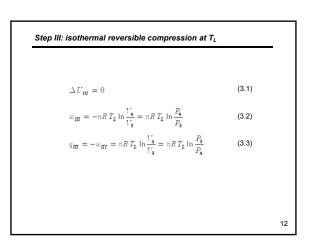


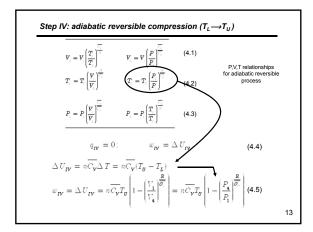


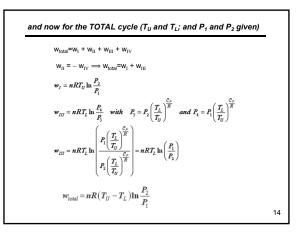
| (see handout "Summary of Heat and Work for the Carnot Cycle Engines, Refrigerators, Heat Pumps") | | | | | | | |
|---|---|---|--|--|--|--|--|
| | | | | | | | |
| ENGINE | a | Wsys | Wsurr | | | | |
| I. isothermal expansion | $+nRT_v \ln \frac{P_1}{P_2}$ 1.3 | $-nRT_v \ln \frac{P_1}{P_2}$ 1.2 | | heat in at T _H work out | | | |
| II adiabatic expansion | 0 | $n\overline{C_V}(T_L - T_V)$ 2.4 | $-n\overline{C_v}(T_L - T_v)$ | work out | | | |
| III. isothermal compression | $\begin{split} & nR T_{\perp} \ln \frac{P_{3}}{P_{4}} = \\ & -nR T_{\perp} \ln \frac{P_{1}}{P_{2}} \\ \end{split} $ | $ \begin{array}{l} -nR T_{\perp} \ln \frac{P_{*}}{P_{*}} \\ = nR T_{\perp} \ln \frac{P_{1}}{P_{2}} \end{array} \qquad \textbf{3.28T.3} \end{array} $ | $-nRT_{\perp}\ln\frac{P_{\perp}}{P_{\perp}}$ | heat lost at T _L work in | | | |
| IV. adiabatic compression | 0 | $n\overline{C_v}(T_v - T_L)$ 4.4 | $-n\overline{C_v}(T_v-T_{\tilde{k}})$ | work in | | | |
| net gain/cost | q _{in} = q _l | | w _{total} = w _l +w _{ll} +w _{lll} +w _{lV} = | ε≡w _{sun} /q _{in} | | | |
| | $+ nR T_v \ln \frac{P_1}{P_2}$ | | $nR(T_v-T_L)\ln\frac{P_1}{P_2}$ | $\epsilon = (T_U - T_L)/T_U$ | | | |
| | 1 | 1 | 1 | | | | |
| | | | | | | | |

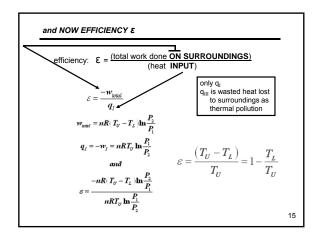












| Engines, Refrigerators, Heat Pumps") | | | | | | | | |
|--------------------------------------|---|---|---|--|--|--|--|--|
| | | | | | | | | |
| ENGINE | q | Wsys | Wsurr | | | | | |
| I. isothermal expansion | $+ nR T_{U} \ln \frac{P_{1}}{P_{2}}$ 1.3 | $-nRT_U \ln \frac{P_1}{P_2}$ 1.2 | $+ nR T_v \ln \frac{P_1}{P_2}$ | heat in at T _H work out | | | | |
| II adiabatic expansion | 0 | $n\overline{C_v}(T_L - T_v)$ 2.4 | $-n\overline{C_v}(T_L - T_v)$ | work out | | | | |
| III. isothermal compression | $nR T_{\perp} \ln \frac{P_{a}}{P_{4}} = $ $-nR T_{\perp} \ln \frac{P_{1}}{P_{2}}$ 3.387.3 | $ \begin{array}{l} -nR T_{\perp} \ln \frac{P_{+}}{P_{+}} \\ = nR T_{\perp} \ln \frac{P_{+}}{P_{2}} \end{array} 3.28 \text{T.3} \end{array} $ | $-nR T_L \ln \frac{P_1}{P_2}$ | heat lost at T _L work in | | | | |
| IV. adiabatic compression | 0 | $n\overline{C_v}(T_v - T_L)$ 4.4 | $-n\overline{C_v}(T_v - T_L)$ | work in | | | | |
| net gain/cost | q _{in} = q ₁ | | w _{total} = w ₁ +w ₁₁ +w ₁₁ +w _{1V} = | E=w _{surr} /q _{in} | | | | |
| | $+ nR T_v \ln \frac{P_1}{P_2}$ | | $nR(T_U - T_L) \ln \frac{P_1}{P_2}$ | $\varepsilon = (T_U - T_L)/T_U$ | | | | |

